





# On the numerical entropy production as a useful mesh refinement parameter: application to wave-breaking.

Mehmet Ersoy<sup>1</sup>, Frédéric Golay<sup>2</sup> and Lyudmyla Yushchenko<sup>3</sup>

University of Sussex, July 24, 2014

- 1. Mehmet.Ersoy@univ-tln.fr
- 2. Frederic.Golay@univ-tln.fr
- 3. Lyudmyla.Yushchenko@univ-tln.fr

# PHYSICAL MODELING AND NUMERICAL MOTIVATION

# **2** 2D and 3D applications

# **③** Concluding Remarks& Perspectives



# Physical modeling and numerical motivation

# 2 2D AND 3D APPLICATIONS

# ③ CONCLUDING REMARKS& PERSPECTIVES

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Application to wave-breaking

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- Shallow water equations : fast but unable to simulate wave breaking
  - Zaleski, Popinet, Diaz, Dutykh, ....



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  - ▶ FV, FE, VOF, level set,  $\ldots$  → accurate but expensive
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- Low-Mach models (Euler equations) : good compromise between physical modeling accuracy and cost



$$\left\{ \begin{array}{l} \displaystyle \frac{\partial \boldsymbol{w}}{\partial t} + \frac{\partial \boldsymbol{f}(\boldsymbol{w})}{\partial x} = 0, \, (t,x) \in \mathbb{R}^+ \times \mathbb{R} \\ \boldsymbol{w}(0,x) = \boldsymbol{w}_0(x), \, x \in \mathbb{R} \end{array} \right.$$

$$oldsymbol{w} \in \mathbb{R}^d$$
 : vector state,

: flux governing the physical description of the flow.

f

$$\begin{cases} \frac{\partial \boldsymbol{w}}{\partial t} + \frac{\partial \boldsymbol{f}(\boldsymbol{w})}{\partial x} = 0, \ (t, x) \in \mathbb{R}^+ \times \mathbb{R} \\ \boldsymbol{w}(0, x) = \boldsymbol{w}_0(x), \ x \in \mathbb{R} \end{cases}$$

Weak solutions satisfy

$$S = \frac{\partial s(\boldsymbol{w})}{\partial t} + \frac{\partial \psi(\boldsymbol{w})}{\partial x} \begin{cases} = 0 & \text{for smooth solution} \\ = 0 & \text{across rarefaction} \\ < 0 & \text{across shock} \end{cases}$$

where  $(s,\psi)$  stands for a convex entropy-entropy flux pair :

$$(\nabla \psi(\boldsymbol{w}))^T = (\nabla s(\boldsymbol{w}))^T \ D_{\boldsymbol{w}} \boldsymbol{f}(\boldsymbol{w})$$

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$$(\nabla \psi_i(\boldsymbol{w}))^T = (\nabla s(\boldsymbol{w}))^T D_{\boldsymbol{w}} \boldsymbol{f}_i(\boldsymbol{w}), \quad i = 1, \dots, d$$

Entropy inequality  $\simeq$  "smoothness indicator"

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#### FINITE VOLUME APPROXIMATION



FIGURE : a cell  $C_k$ 

Finite volume approximation :

$$\boldsymbol{w}_{k}^{n+1} = \boldsymbol{w}_{k}^{n} - \frac{\delta t_{n}}{h_{k}} \left( \boldsymbol{F}_{k+1/2}^{n} - \boldsymbol{F}_{k-1/2}^{n} \right)$$

$$\boldsymbol{w}_{k}^{n} \simeq \frac{1}{h_{k}} \int_{C_{k}} \boldsymbol{w}\left(t_{n}, x\right) \, dx$$

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The numerical density of entropy production :

$$S_{k}^{n} = \frac{s_{k}^{n+1} - s_{k}^{n}}{\delta t_{n}} + \frac{\psi_{k+1/2}^{n} - \psi_{k-1/2}^{n}}{h_{k}} \lessapprox 0$$

• Compute  $w_k^n$ 

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  - ★ hierarchical numbering : basis 2



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0	10	11
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2	3	

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#### ONE-DIMENSIONAL GAS DYNAMICS EQUATIONS FOR IDEAL GAS

$$\begin{split} \frac{\partial \rho}{\partial t} &+ \frac{\partial \rho u}{\partial x} = 0\\ \frac{\partial \rho u}{\partial t} &+ \frac{\partial \left(\rho u^2 + p\right)}{\partial x} = 0 \quad \text{where} \\ \frac{\partial \rho E}{\partial t} &+ \frac{\partial \left(\rho E + p\right) u}{\partial x} = 0\\ p &= (\gamma - 1)\rho\varepsilon \end{split}$$

$$\begin{array}{rcl} \rho(t,x) & : & \text{density} \\ u(t,x) & : & \text{velocity} \\ p(t,x) & : & \text{pressure} \\ \gamma := 1.4 & : & \text{ratio of} \\ E(\varepsilon,u) & : & \text{total end} \\ \varepsilon & : & \text{internal} \\ E & = & \varepsilon + \frac{u^2}{2} \end{array}$$

- of the specific heats
- energy
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Intel(R) Core(TM) i5-2500 CPU @ 3.30GHz

#### ONE-DIMENSIONAL GAS DYNAMICS EQUATIONS FOR IDEAL GAS

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} = 0 \qquad \begin{array}{c} \rho(t, x) & \vdots \\ u(t, x) & \vdots \\ p(t, x) & \vdots \\ p(t$$

$$\begin{array}{rcl} x) & : & \text{density} \\ x) & : & \text{velocity} \\ x) & : & \text{pressure} \\ = 1.4 & : & \text{ratio of the specific heats} \\ , u) & : & \text{total energy} \\ & : & \text{internal specific energy} \\ & = & \varepsilon + \frac{u^2}{2} \end{array}$$

• Conservative variables

$$\boldsymbol{w} = \left(\rho, \rho u, \rho E\right)^t$$

convex continuous entropy

$$s(\boldsymbol{w}) = -\rho \ln \left( rac{p}{
ho^{\gamma}} 
ight)$$
 of flux  $\psi(\boldsymbol{w}) = u \, s(\boldsymbol{w})$ 

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#### SOD'S SHOCK TUBE PROBLEM

Mesh refinement parameter  $\alpha_{max}$ 0.01, Mesh coarsening parameter  $\alpha_{\min}$ 0.001, : Mesh refinement parameter  $\bar{S}$  $\Omega$ CFL 0.25,٠ Simulation time (s)0.4,Initial number of cells 200,Maximum level of mesh refinement  $L_{\max}$ .



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#### ACCURACY



(a) Density and numerical density of en- (b) Mesh refinement level, numerical tropy production. density of entropy production and local error.

FIGURE : Sod's shock tube problem : solution at time t=0.4 s using the AB1M scheme on a dynamic grid with  $L_{\rm max}=5$  and the AB1 scheme on a uniform fixed grid of 681 cells.

### Shu and Osher test case



# Reference solution&Numerical results



FIGURE : Shu and Osher test case.

### TIME RESTRICTION

• Explicit adaptive schemes : time consuming due to the restriction

$$\|w\|\frac{\delta}{h} \leqslant 1, \quad h = \min_k h_k$$



Müller S., Stiriba Y., SIAM J. Sci. Comput., (07); Ersoy M., Golay F., Yushchenko L., CEJM, (13);

#### TIME RESTRICTION, LOCAL TIME STEPPING APPROACH

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  - Sort cells in groups w.r.t. to their level

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#### TIME RESTRICTION, LOCAL TIME STEPPING APPROACH & AIMS

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  - Update the cells following the local time stepping algorithm.

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FIGURE : 
$$t = t_n$$

$$\delta F_{k-1,k,k+1}^n := \left( F_{k+1/2}^n(w_k, w_{k+1}) - F_{k-1/2}^n(w_{k-1}, w_k) \right)$$



FIGURE : 
$$t_{n_1} = t_n + \delta t_n$$

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FIGURE : 
$$\iota_{n_2} = \iota_n + 20\iota_n$$
  
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1 954

1

ELCUIDE . 4



FIGURE : 
$$t_{n_3} = t_n + 3\delta t_n$$

$$\delta F_{k-1,k,k+1}^n := \left( \boldsymbol{F}_{k+1/2}^n(\boldsymbol{w}_k, \boldsymbol{w}_{k+1}) - \boldsymbol{F}_{k-1/2}^n(\boldsymbol{w}_{k-1}, \boldsymbol{w}_k) \right)$$
### ILLUSTRATION



#### LOCAL TIME STEPPING ALGORITHM



	$\mathcal{P}$	$\ \rho - \rho_{ref}\ _{l^1_x}$	cpu-time	$N_{L_{\max}}$	maximum number of cells
AB1	0.288	$4.7410^{-2}$	181	1574	2308

 $\operatorname{TABLE}$  : Shu and Osher test case : comparison of numerical schemes of order 1

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RK2	0.285	$2.0810^{-2}$	299	1375	2005

 $\operatorname{TABLE}$  : Shu and Osher test case : comparison of numerical schemes of order 1 and 2

### Properties

In particular, one has :

# THEOREM

Consider a  $p^{\text{th}}$  convergent scheme. Let  $S_k^n$  be the corresponding numerical density of entropy production and  $\Delta t = \lambda h$  be a fixed time step where h stands for the meshsize.

Then

$$\lim_{n \to \infty} S_k^n = \begin{cases} O(\Delta t^p) \\ O\left(\frac{1}{\Delta t}\right) \end{cases}$$

if the solution is smooth,

if the solution is discontinuous.

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Consider a monotone scheme. Then, for almost every k, every n,

 $S_k^n \leqslant 0.$ 

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# PROPERTIES

Consider a monotone scheme. Then, for almost every k, every n,

 $S_k^n \leqslant 0.$ 

Thus, even if locally  $S_k^n$  can take positive value, one has  $S_k^n \leqslant C\Delta t^q$ ,  $q \ge p$ .

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Let us consider the transport equation :

$$\begin{cases} w_t + w_x &= 0\\ w(0, x) &= w_0(x) \end{cases}$$

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with  $s(w)=w^2$  and  $\psi(w)=w^2.$ 

Substituting  $w_k^{n+1}$  into  $S_k^{n+1}$ , we get

$$S_k^{n+1} = -\varepsilon \left(\frac{w_k^n - w_{k-1}^n}{\delta x}\right)^2 \leq 0 \text{ with } \varepsilon = \delta x \left(1 - \frac{\delta t}{\delta x}\right) > 0.$$

### 123 problem

CFL	:	0.25,
Simulation time $(s)$	:	0.15,
Initial number of cells	:	200,
Maximum level of mesh refinement	:	4.



# 123 problem



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# 123 problem



FIGURE : Test 2 :  $\|\varepsilon - \varepsilon_{ex}\|_{l^1_x}$  with respect to the average number of cells at time t = 0.15.

# The blast wave problem

CFL	:	0.25,
Simulation time $(s)$	:	0.038,
Initial number of cells	:	200,
Maximum level of mesh refinement	:	$L_{\max}$ .



#### THE BLAST WAVE PROBLEM



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## THE BLAST WAVE PROBLEM



FIGURE :  $\|\varepsilon - \varepsilon_{ex}\|_{l^1_{x}}$  with respect to the average number of cells at time t = 0.038.



# **D** Physical modeling and numerical motivation

# **2** 2D and 3D applications

# ③ CONCLUDING REMARKS& PERSPECTIVES

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Application to wave-breaking

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Kleefsmann (ComFlow)

 NS+VOF+Surface tension MAC Golay 0.8M cells Bifluid Euler FV 2days CPU M=0.1 1 day CPU M=0.2

Cm2





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• Model (2D and 3D) : low mach bi-fluid euler

$$\begin{split} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 & \rho(t, x) \\ u(t, x) & u(t, x) \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g & p(t, x) \\ \frac{\partial \rho E}{\partial t} + \operatorname{div}((\rho E + p) u) &= 0 & \varepsilon \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 & E \end{split}$$

- : density
- : velocity
- : pressure
- : total energy
- : internal specific energy
- fluid's fraction

$$= \varepsilon + \frac{u^2}{2}$$

• Model (2D and 3D) : low mach bi-fluid euler

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• Mach number  $< 0.3 \rightarrow$  fluid is slightly compressible

• Model (2D and 3D) : low mach bi-fluid euler

$$\begin{split} \frac{\partial\rho}{\partial t} + \operatorname{div}(\rho u) &= 0 & \begin{array}{ccc} \rho(t,x) & : & \operatorname{density} \\ u(t,x) & : & \operatorname{velocity} \\ p(t,x) & : & \operatorname{pressure} \\ \hline \partial \rho u \\ \frac{\partial\rho u}{\partial t} + \operatorname{div}\left(\rho u^2 + pI\right) &= \rho g \\ \text{where} & E(\varepsilon,u) & : & \operatorname{total energy} \\ \hline \partial \rho E \\ \frac{\partial\rho E}{\partial t} + \operatorname{div}\left((\rho E + p) u\right) &= 0 & \begin{array}{ccc} \varepsilon & : & \operatorname{internal specific energy} \\ \varphi & : & \operatorname{fluid's fraction} \\ \hline & \frac{\partial\varphi}{\partial t} + u \cdot \nabla\varphi &= 0 \end{array}$$

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with

$$p = p_0 + c_0 \left( \rho - (\varphi \rho_w + (1 - \varphi) \rho_a) \right)$$

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- Explicit scheme  $\rightarrow$  easy parallel implementation (MPI)
- Equation of state with artificial sound speed → CFL less restrictive M. Ersoy (IMATH) Application to wave-breaking University of Sussex, July 24, 2014

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# hyperbolic system

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hyperbolic system  $\checkmark$ entropy available

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 $\overline{\checkmark}$ 

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with

$$p = p_0 + c_0 \left(\rho - \left(\varphi \rho_w + (1 - \varphi)\rho_a\right)\right)$$

hyperbolic system

• Moreover,

- entropy available
- automatic mesh refinement

 $\checkmark$ 

 $\overline{\checkmark}$ 

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- entropy available
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- local time stepping

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 $\overline{\checkmark}$ 

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  - It certainly exists better strategy ...
- Management of domain's interfaces, projection step, ...



How it works?

• each domain has almost the same number of cells

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# 2D-3D DAMBREAK WITH AN OBSTACLE





(top left : mesh, top middle :  $\rho$ , top right :  $S_k^n$ , bottom left : level, bottom right :  $\frac{1}{|D|} \int_D S_k^n$ )

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# VERSUS EXPRIMENTAL (KOSHIZUKA, TAMAKO, OKA, 95)

$$T = 0.2s$$

$$T = 0.3s$$

$$T = 0.4s$$

$$T = 0.2s$$

# KLEEFSMANN TEST CASE

- 10h cpu (instead of 1 day)
- 48 cpus, 48 domains, 3628 blocks
- transfer and post-processing take more time!





#### JUST FOR FUN : VISUALISATION TOOL

- povray = Persistence Of Vision RAYtracer : high quality and realistic picture
- Povray postprocess is expensive but the results are beautiful !!!
- first movie (Shallow water equations with a moving bed) :



- each picture  $\approx$  6Mo
- time to generate 1 picture pprox 10 min
- here 500 picture ...

• A second movie (bifluid Euler equations) :



- 4 level
- 20 domains
- 100 time step
- $\alpha_{\min} = 0.02$ ,  $\alpha_{\max} = 0.2$
- 172 215 587763 cells
- 7h computation

• speed-up vs proc number



• cpu time vs proc number



# • Riemann data :

$$(p,\rho,u,v)(0,x,y) = \begin{cases} (p_1,\rho_1,u_1,v_1), & \text{if } x > 0.5 & \text{and } y > 0.5\\ (p_2,\rho_2,u_2,v_2), & \text{if } x < 0.5 & \text{and } y > 0.5\\ (p_3,\rho_3,u_3,v_3), & \text{if } x < 0.5 & \text{and } y < 0.5\\ (p_4,\rho_4,u_4,v_4), & \text{if } x > 0.5 & \text{and } y < 0.5 \end{cases}$$

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• 19 possible configuration : forward or backward 1 D waves (rarefaction, shock and contact discontinuity)

# • Riemann data :

$$(p,\rho,u,v)(0,x,y) = \begin{cases} (0.4,0.5313,0,0), & \text{if } x > 0.5 & \text{and } y > 0.5\\ (1,1,0.7276,0), & \text{if } x < 0.5 & \text{and } y > 0.5\\ (1,0.8,0,0), & \text{if } x < 0.5 & \text{and } y < 0.5\\ (1,1,0,0), & \text{if } x > 0.5 & \text{and } y < 0.5 \end{cases}$$

# • Resolution of stationary contacts bordering the lower left quadrant



# • Riemann data :

$$(p,\rho,u,v)(0,x,y) = \begin{cases} (1,1,0,-0.4), & \text{if } x > 0.5 & \text{and } y > 0.5\\ (1,2,0,-0.3), & \text{if } x < 0.5 & \text{and } y > 0.5\\ (0.4,1.0625,0,0.2145), & \text{if } x < 0.5 & \text{and } y < 0.5\\ (0.4,0.5197,0,-1.1259), & \text{if } x > 0.5 & \text{and } y < 0.5 \end{cases}$$

# • Two standing contacts on the line x=0.5





# PHYSICAL MODELING AND NUMERICAL MOTIVATION

# 2 2D AND 3D APPLICATIONS

# **3** Concluding Remarks& Perspectives

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Application to wave-breaking

University of Sussex, July 24, 2014 36 / 38

## Achievements and perspectives in CM2

• low mach bi-fluid model 1D, 2D and 3D

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►

## Thank you

### for your

# attention

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