

Block-Based Adaptive Mesh Refinement scheme based on numerical density of entropy production for conservation laws and applications.

Mehmet Ersoy¹,

Frédéric Golay, Lyudmyla Yushchenko, Université de Toulon, IMATH,
and Damien Sous, Aix-Marseille Université, CNRS/INSU, IRD, MIO

International meeting AMS/EMS/SPM

Partial Differential Equations: Ambitious Mathematics for Real-life Applications

2015, 10-13 June, Porto, Portugal

- **Physical motivations** : to be able to simulate applications in real-life fluid mechanics in dimension 2 and 3
 - ▶ wave-breaking,
 - ▶ wave-impacting,
 - ▶ tsunami ...

- **Physical motivations** : to be able to simulate applications in real-life fluid mechanics in dimension 2 and 3
 - ▶ wave-breaking,
 - ▶ wave-impacting,
 - ▶ tsunami ...
- **Numerical motivations** : to be able to design a model and a numerical code for such applications
 - ▶ fast and accurate,
 - ▶ limiting the numerical diffusion,
 - ▶ adaptive and a suitable meshing machinery,
 - ▶ optimized numerical code,
 - ▶ ...

- **Physical motivations** : to be able to simulate applications in real-life fluid mechanics in dimension 2 and 3
 - ▶ wave-breaking,
 - ▶ wave-impacting,
 - ▶ tsunami ...
- **Numerical motivations** : to be able to design a model and a numerical code for such applications
 - ▶ fast and accurate,
 - ▶ limiting the numerical diffusion,
 - ▶ adaptive and a suitable meshing machinery,
 - ▶ optimized numerical code,
 - ▶ ...
- **Mathematical motivations** : introducing new tools
 - ▶ a suitable mesh refinement tool and its mathematical properties
 - ▶ consistency at interface of two cells of different level,
 - ▶ ...

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

We focus on general **non linear hyperbolic conservation laws**

$$\begin{cases} \frac{\partial \mathbf{w}}{\partial t} + \frac{\partial \mathbf{f}(\mathbf{w})}{\partial x} = 0, (t, x) \in \mathbb{R}^+ \times \mathbb{R} \\ \mathbf{w}(0, x) = \mathbf{w}_0(x), x \in \mathbb{R} \end{cases}$$

$\mathbf{w} \in \mathbb{R}^d$: vector state,

\mathbf{f} : flux governing the physical description of the flow.

We focus on general **non linear hyperbolic conservation laws**

$$\begin{cases} \frac{\partial \mathbf{w}}{\partial t} + \frac{\partial \mathbf{f}(\mathbf{w})}{\partial x} = 0, (t, x) \in \mathbb{R}^+ \times \mathbb{R} \\ \mathbf{w}(0, x) = \mathbf{w}_0(x), x \in \mathbb{R} \end{cases}$$

Weak solutions satisfy

$$S = \frac{\partial s(\mathbf{w})}{\partial t} + \frac{\partial \psi(\mathbf{w})}{\partial x} \begin{cases} = 0 & \text{for smooth solution} \\ = 0 & \text{across rarefaction} \\ < 0 & \text{across shock} \end{cases}$$

where (s, ψ) stands for a **convex entropy-entropy flux pair** :

$$(\nabla \psi(\mathbf{w}))^T = (\nabla s(\mathbf{w}))^T D_{\mathbf{w}} \mathbf{f}(\mathbf{w})$$

We focus on general **non linear hyperbolic conservation laws**

$$\begin{cases} \frac{\partial \mathbf{w}}{\partial t} + \frac{\partial \mathbf{f}(\mathbf{w})}{\partial x} = 0, (t, x) \in \mathbb{R}^+ \times \mathbb{R} \\ \mathbf{w}(0, x) = \mathbf{w}_0(x), x \in \mathbb{R} \end{cases}$$

Weak solutions satisfy

$$S = \frac{\partial s(\mathbf{w})}{\partial t} + \frac{\partial \psi(\mathbf{w})}{\partial x} \begin{cases} = 0 & \text{for smooth solution} \\ = 0 & \text{across rarefaction} \\ < 0 & \text{across shock} \end{cases}$$

where (s, ψ) stands for a **convex entropy-entropy flux pair** :

$$(\nabla \psi(\mathbf{w}))^T = (\nabla s(\mathbf{w}))^T D_{\mathbf{w}} \mathbf{f}(\mathbf{w})$$

Entropy inequality \simeq “**smoothness indicator**”



Croisille J.-P., *Contribution à l'Étude Théorique et à l'Approximation par Éléments Finis du Système Hyperbolique de la Dynamique des Gaz Multidimensionnelle et Multiespèces*, PhD thesis, Université de Paris VI, 1991

We focus on general **non linear hyperbolic conservation laws**

$$\begin{cases} \frac{\partial \mathbf{w}}{\partial t} + \operatorname{div}(\mathbf{f}(\mathbf{w})) = 0, (t, x) \in \mathbb{R}^+ \times \mathbb{R}^m \\ \mathbf{w}(0, x) = \mathbf{w}_0(x), x \in \mathbb{R}^m \end{cases}$$

Weak solutions satisfy

$$S = \frac{\partial s(\mathbf{w})}{\partial t} + \operatorname{div}(\psi(\mathbf{w})) \begin{cases} = 0 & \text{for smooth solution} \\ = 0 & \text{across rarefaction} \\ < 0 & \text{across shock} \end{cases}$$

where (s, ψ) stands for a **convex entropy-entropy flux pair** :

$$(\nabla \psi_i(\mathbf{w}))^T = (\nabla s(\mathbf{w}))^T D_{\mathbf{w}} \mathbf{f}_i(\mathbf{w}), \quad i = 1, \dots, d$$

Entropy inequality \simeq “**smoothness indicator**”



Croisille J.-P., *Contribution à l'Étude Théorique et à l'Approximation par Éléments Finis du Système Hyperbolique de la Dynamique des Gaz Multidimensionnelle et Multiespèces*, PhD thesis, Université de Paris VI, 1991

FINITE VOLUME APPROXIMATION

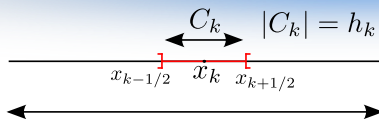


FIGURE: a cell C_k

Finite volume approximation :

$$\mathbf{w}_k^{n+1} = \mathbf{w}_k^n - \frac{\delta t_n}{h_k} \left(\mathbf{F}_{k+1/2}^n - \mathbf{F}_{k-1/2}^n \right)$$

with

$$\mathbf{w}_k^n \simeq \frac{1}{h_k} \int_{C_k} \mathbf{w}(t_n, x) \, dx \text{ and } \mathbf{F}_{k+1/2}^n \approx \frac{1}{\delta t} \int_{C_k} \mathbf{f}(t, w(t, x_{k+1/2})) \, dx$$

FINITE VOLUME APPROXIMATION

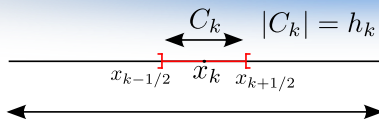


FIGURE: a cell C_k

Finite volume approximation :

$$\mathbf{w}_k^{n+1} = \mathbf{w}_k^n - \frac{\delta t_n}{h_k} \left(\mathbf{F}_{k+1/2}^n - \mathbf{F}_{k-1/2}^n \right)$$

with

$$\mathbf{w}_k^n \simeq \frac{1}{h_k} \int_{C_k} \mathbf{w}(t_n, x) dx \text{ and } \mathbf{F}_{k+1/2}^n \approx \frac{1}{\delta t} \int_{C_k} \mathbf{f}(t, w(t, x_{k+1/2})) dx$$

The numerical density of entropy production :

$$S_k^n = \frac{s_k^{n+1} - s_k^n}{\delta t_n} + \frac{\psi_{k+1/2}^n - \psi_{k-1/2}^n}{h_k} \lesssim 0$$

FINITE VOLUME APPROXIMATION

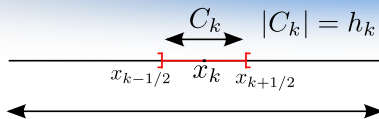


FIGURE: a cell C_k

Finite volume approximation :

$$\mathbf{w}_k^{n+1} = \mathbf{w}_k^n - \frac{\delta t_n}{h_k} \left(\sum_a \mathbf{F}(\mathbf{w}_k^n, \mathbf{w}_a^n; n_{k/a}) \right), \quad h_k = \frac{|C_k|}{\sum_a |\partial C_{k/a}|}$$

with

$$\mathbf{w}_k^n \simeq \frac{1}{h_k} \int_{C_k} \mathbf{w}(t_n, x) \, dx, \quad \text{and} \quad \mathbf{F}(\mathbf{w}_k^n, \mathbf{w}_a^n; n_{k/a}) \approx \frac{1}{\delta t} \int_{\partial C_k} \mathbf{f}(t, \mathbf{w}) \cdot \mathbf{n}_{k/a} \, ds$$

FINITE VOLUME APPROXIMATION

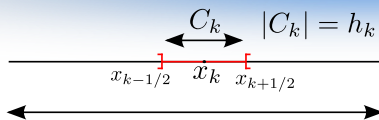


FIGURE: a cell C_k

Finite volume approximation :

$$\mathbf{w}_k^{n+1} = \mathbf{w}_k^n - \frac{\delta t_n}{h_k} \left(\sum_a \mathbf{F}(\mathbf{w}_k^n, \mathbf{w}_a^n; n_{k/a}) \right), \quad h_k = \frac{|C_k|}{\sum_a |\partial C_{k/a}|}$$

with

$$\mathbf{w}_k^n \simeq \frac{1}{h_k} \int_{C_k} \mathbf{w}(t_n, x) dx, \quad \text{and} \quad \mathbf{F}(\mathbf{w}_k^n, \mathbf{w}_a^n; n_{k/a}) \approx \frac{1}{\delta t} \int_{\partial C_k} \mathbf{f}(t, \mathbf{w}) \cdot \mathbf{n}_{k/a} ds$$

The numerical density of entropy production :

$$S_k^n = \frac{s_k^{n+1} - s_k^n}{\delta t_n} + \frac{\sum_a \psi(\mathbf{w}_k^n, \mathbf{w}_a^n; n_{k/a})}{h_k} \lesssim 0$$

MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}

MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- **Compute** S_k^n : $S_k^n \neq 0 \implies$ the cell is refined or coarsened

MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

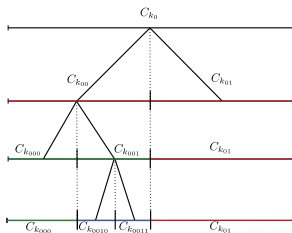
- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \implies$ the cell is refined or coarsened
- More precisely :
 - ▶ $S_k^n \leq \alpha_{\min} \bar{S} \implies$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$

MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \implies$ the cell is refined or coarsened
- More precisely :
 - ▶ $S_k^n \leq \alpha_{\min} \bar{S} \implies$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - ▶ $S_k^n \geq \alpha_{\max} \bar{S} \implies$ the cell is coarsened

MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute S_k^n : $S_k^n \neq 0 \Rightarrow$ the cell is refined or coarsened
- **More precisely :**
 - ▶ $S_k^n \leq \alpha_{\min} \bar{S} \Rightarrow$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - ▶ $S_k^n \geq \alpha_{\max} \bar{S} \Rightarrow$ the cell is coarsened
 - ▶ **Dynamic mesh refinement :**
 - ★ **Dyadic tree (1D)**
 - ★ hierarchical numbering : basis 2



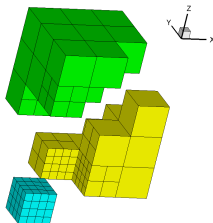
MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \implies$ the cell is refined or coarsened
- **More precisely :**
 - ▶ $S_k^n \leq \alpha_{\min} \bar{S} \implies$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - ▶ $S_k^n \geq \alpha_{\max} \bar{S} \implies$ the cell is coarsened
 - ▶ **Dynamic mesh refinement :**
 - ★ Non-structured grid : macro-cell
 - ★ Dyadic tree (1D), **Quadtree (2D)**
 - ★ hierarchical numbering : basis 2,4

0	10		11
	120	121	13
	122	123	
2	3		

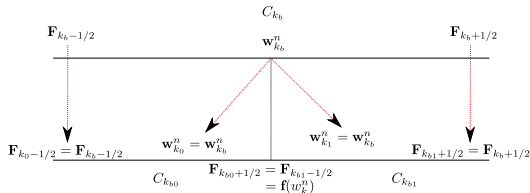
MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \implies$ the cell is refined or coarsened
- **More precisely :**
 - ▶ $S_k^n \leq \alpha_{\min} \bar{S} \implies$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - ▶ $S_k^n \geq \alpha_{\max} \bar{S} \implies$ the cell is coarsened
 - ▶ **Dynamic mesh refinement :**
 - ★ **Non-structured grid : macro-cell**
 - ★ Dyadic tree (1D), Quadtree (2D), **Octree (3D)**
 - ★ hierarchical numbering : basis 2,4,8



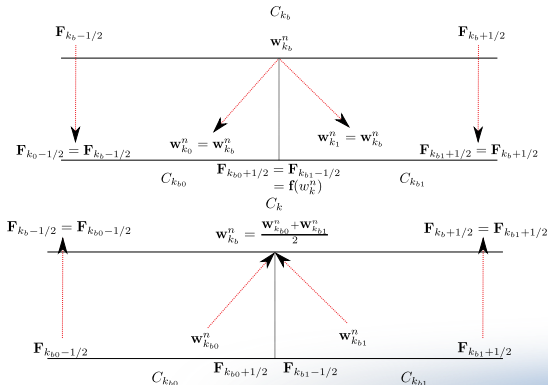
MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \Rightarrow$ the cell is refined or coarsened
- More precisely :
 - $S_k^n \leq \alpha_{\min} \bar{S} \Rightarrow$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - $S_k^n \geq \alpha_{\max} \bar{S} \Rightarrow$ the cell is coarsened



MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute S_k^n : $S_k^n \neq 0 \Rightarrow$ the cell is refined or coarsened
- More precisely :
 - $S_k^n \leq \alpha_{\min} \bar{S} \Rightarrow$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - $S_k^n \geq \alpha_{\max} \bar{S} \Rightarrow$ the cell is coarsened



MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \implies$ the cell is refined or coarsened
- **More precisely :**
 - ▶ $S_k^n \leq \alpha_{\min} \bar{S} \implies$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - ▶ $S_k^n \geq \alpha_{\max} \bar{S} \implies$ the cell is coarsened
 - ▶ Simple approach **but** the scheme is locally non consistent [SO88, TW05]



Shu C. W., Osher S., *Efficient implementation of essentially nonoscillatory shock-capturing schemes*. J. Comput. Phys., 77(2) :439–471, 1988.



Tang H., Warnecke G., *A class of high resolution difference schemes for nonlinear Hamilton-Jacobi equations with varying time and space grids*. SIAM J. Sci. Comput., 26(4) :1415–1431, 2005.

MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \implies$ the cell is refined or coarsened
- More precisely :
 - ▶ $S_k^n \leq \alpha_{\min} \bar{S} \implies$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
 - ▶ $S_k^n \geq \alpha_{\max} \bar{S} \implies$ the cell is coarsened
 - ▶ Simple approach **but** the scheme is locally non consistent [SO88, TW05]
 - ▶ Limit the mesh level of adjacent cells by 2



Shu C. W., Osher S., *Efficient implementation of essentially nonoscillatory shock-capturing schemes*. J. Comput. Phys., 77(2) :439–471, 1988.



Tang H., Warnecke G., *A class of high resolution difference schemes for nonlinear Hamilton-Jacobi equations with varying time and space grids*. SIAM J. Sci. Comput., 26(4) :1415–1431, 2005.

MESH REFINEMENT INDICATOR : PRINCIPLE & ILLUSTRATION

- Given $w_k^n \rightarrow$ compute w_k^{n+1}
- Compute $S_k^n : S_k^n \neq 0 \implies$ the cell is refined or coarsened
- **More precisely :**

- ▶ $S_k^n \leq \alpha_{\min} \bar{S} \implies$ the cell is refined with $\bar{S} = \frac{1}{|\Omega|} \int_{\Omega} S_k^n$
- ▶ $S_k^n \geq \alpha_{\max} \bar{S} \implies$ the cell is coarsened
- ▶ Simple approach **but** the scheme is locally non consistent [SO88, TW05]
- ▶ Limit the mesh level of adjacent cells by 2
- ▶ A correction can be obtained (work in progress) [AE15]



Altazin T., Ersoy, M. *Analyze of the inconsistency of adaptive scheme. Preprint (in progress)*, 2015.



Shu C. W., Osher S., *Efficient implementation of essentially nonoscillatory shock-capturing schemes*. J. Comput. Phys., 77(2) :439–471, 1988.



Tang H., Warnecke G., *A class of high resolution difference schemes for nonlinear Hamilton-Jacobi equations with varying time and space grids*. SIAM J. Sci. Comput., 26(4) :1415–1431, 2005.

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

AN EXAMPLE : THE ONE-DIMENSIONAL GAS DYNAMICS EQUATIONS FOR IDEAL GAS

$$\begin{aligned}\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} &= 0 \\ \frac{\partial \rho u}{\partial t} + \frac{\partial (\rho u^2 + p)}{\partial x} &= 0 \quad \text{where} \\ \frac{\partial \rho E}{\partial t} + \frac{\partial (\rho E + p) u}{\partial x} &= 0 \\ p &= (\gamma - 1) \rho \varepsilon\end{aligned}$$

$\rho(t, x)$:	density
$u(t, x)$:	velocity
$p(t, x)$:	pressure
$\gamma := 1.4$:	ratio of the specific heats
$E(\varepsilon, u)$:	total energy
ε	:	internal specific energy
E	=	$\varepsilon + \frac{u^2}{2}$

AN EXAMPLE : THE ONE-DIMENSIONAL GAS DYNAMICS EQUATIONS FOR IDEAL GAS

$$\begin{aligned}\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} &= 0 \\ \frac{\partial \rho u}{\partial t} + \frac{\partial (\rho u^2 + p)}{\partial x} &= 0 \quad \text{where} \\ \frac{\partial \rho E}{\partial t} + \frac{\partial (\rho E + p) u}{\partial x} &= 0 \\ p &= (\gamma - 1) \rho \varepsilon\end{aligned}$$

$\rho(t, x)$:	density
$u(t, x)$:	velocity
$p(t, x)$:	pressure
$\gamma := 1.4$:	ratio of the specific heats
$E(\varepsilon, u)$:	total energy
ε	:	internal specific energy
E	=	$\varepsilon + \frac{u^2}{2}$

- Conservative variables

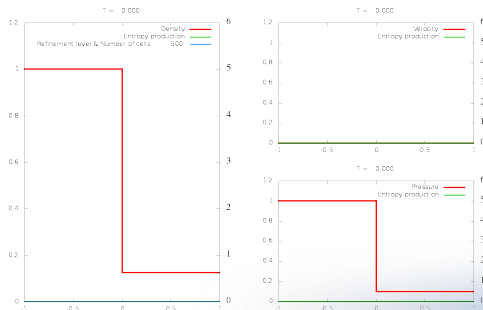
$$\mathbf{w} = (\rho, \rho u, \rho E)^t$$

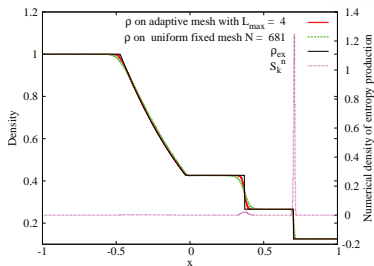
- entropy

$$s(\mathbf{w}) = -\rho \ln \left(\frac{p}{\rho^\gamma} \right) \quad \text{of flux } \psi(\mathbf{w}) = u s(\mathbf{w}) .$$

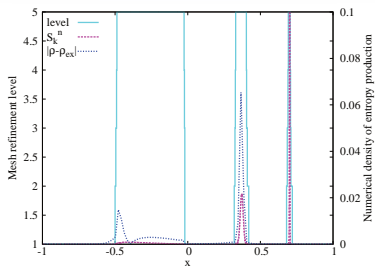
SOD'S SHOCK TUBE PROBLEM

Mesh refinement parameter α_{\max}	:	0.01 ,
Mesh coarsening parameter α_{\min}	:	0.001 ,
Mesh refinement parameter \bar{S}	:	$\frac{1}{ \Omega } \sum_{k_b} S_{k_b}^n$
CFL	:	0.25,
Simulation time (s)	:	0.4,
Initial number of cells	:	200,
Maximum level of mesh refinement	:	L_{\max} .





(a) Density and numerical density of entropy production.



(b) Mesh refinement level, numerical density of entropy production and local error.

FIGURE: Sod's shock tube problem : solution at time $t = 0.4$ s using the AB1M scheme on a dynamic grid with $L_{\max} = 5$ and the AB1 scheme on a uniform fixed grid of 681 cells.

- Explicit adaptive schemes : **time consuming** due to the restriction

$$\|w\| \frac{\delta t}{h} \leq 1, \quad h = \min_k h_k$$

- Explicit adaptive schemes : time consuming due to the restriction

$$\|w\| \frac{\delta t}{h} \leq 1, \quad h = \min_k h_k$$

- Local time stepping algorithm :
 - ▶ Sort cells in groups w.r.t. to their level



Muller S., Stiriba Y., *Fully adaptive multiscale schemes for conservation laws employing locally varying time stepping*. SIAM J. Sci. Comput., 30(3) :493–531, 2007.

- Explicit adaptive schemes : time consuming due to the restriction

$$\|w\| \frac{\delta t}{h} \leq 1, \quad h = \min_k h_k$$

- Local time stepping algorithm :
 - ▶ Sort cells in groups w.r.t. to their level
 - ▶ Update the cells following the local time stepping algorithm.



Muller S., Stiriba Y., *Fully adaptive multiscale schemes for conservation laws employing locally varying time stepping*. SIAM J. Sci. Comput., 30(3) :493–531, 2007.

- Explicit adaptive schemes : time consuming due to the restriction

$$\|w\| \frac{\delta t}{h} \leq 1, \quad h = \min_k h_k$$

- Local time stepping algorithm :
 - ▶ Sort cells in groups w.r.t. to their level
 - ▶ Update the cells following the local time stepping algorithm.
 - ▶ **save the cpu-time keeping the accuracy.**



M. Ersoy, F. Golay, L. Yushchenko. *Adaptive multi-scale scheme based on numerical entropy production for conservation laws*. CEJM, Central European Journal of Mathematics, 11(8), pp 1392-1415, 2013.



M. Ersoy, F. Golay, L. Yushchenko. Adaptive scheme based on entropy production : robustness through severe test cases for hyperbolic conservation laws. *Preprint*, <https://hal.archives-ouvertes.fr/hal-00918773>, 2013.

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

- Main difficulty : mesh and data structure.

For fast computation, the following are required

- ▶ parallel treatment
- ▶ hierarchical grids

- Main difficulty : mesh and data structure.

Some interesting issues :

- ▶ 2D quad-tree [ZW11],
- ▶ 3D octree [LGF04],
- ▶ 2D/3D anisotropic AMR [HFCC13].



Zhang, M., and W.M. Wu. 2011. *A two dimensional hydrodynamic and sediment transport model for dam break based on finite volume method with quadtree grid*. Applied Ocean Research 33 (4) : 297 – 308.



Losasso, F., F. Gibou, and R. Fedkiw. 2004. *Simulating Water and Smoke with an Octree Data Structure*. ACM Trans. Graph. 23 (3) : 457–462, 2004.



Hachem, E., S. Feghali, R. Codina, and T. Coupez. *Immersed stress method for fluid structure interaction using anisotropic mesh adaptation*. International Journal for Numerical Methods in Engineering 94 (9) : 805–825, 2013.

TWO AND THREE DIMENSIONAL CASE : BB-AMR

- Main difficulty : mesh and data structure.
- The strategy adopted :

TWO AND THREE DIMENSIONAL CASE : BB-AMR

- Main difficulty : mesh and data structure.
- The strategy adopted :
 - ① 1 fixed domain= 1 fixed block=1 cpu : “failure” → synchronization depends on the finest domain

- Main difficulty : mesh and data structure.
- The strategy adopted :
 - 1 fixed domain= 1 fixed block=1 cpu : “failure” → synchronization depends on the finest domain
 - 1 dynamic domain= $n \times \text{static blocks} = 1\text{cpu}$: “good compromise” → each domain has almost the same number of cells → “better”
synchronization = Block-Based Adaptive Mesh Refinement (BB-AMR)

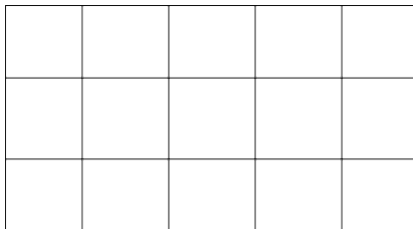
- Main difficulty : mesh and data structure.
- The strategy adopted :
 - ❶ 1 fixed domain= 1 fixed block=1 cpu : “failure” → synchronization depends on the finest domain
 - ❷ 1 dynamic domain= $n \times$ static blocks = 1cpu : “good compromise” → each domain has almost the same number of cells → “better”
synchronization = Block-Based Adaptive Mesh Refinement (BB-AMR)
 - ❸ It certainly exists better strategy ...

How it works?

- each domain has almost the same number of cells

How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering



How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering

6	9			
3	5	8		
1	2	4	7	

How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering

6	9			
D_1	5	8		
		4	7	

How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering

3	6	9		
D_1	2	5	8	
		1	4	7

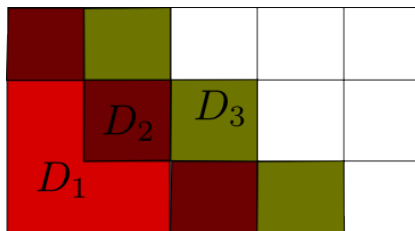
How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering

	6	9		
	D_2	5	8	
D_1			4	7

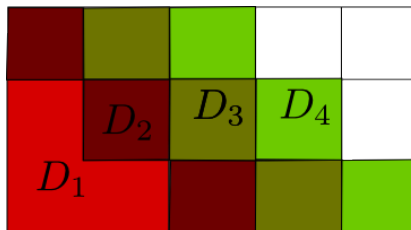
How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering



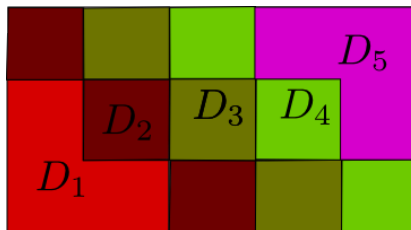
How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering



How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering



How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering
- more sophisticated numbering exists . . .

How it works ?

- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering
- more sophisticated numbering exists . . .
- re-numbering and re-meshing being expensive
 - ▶ the mesh should be kept constant on a time interval

How it works ?

- each domain has almost the same number of cells
 - domain are defined using Cuthill-McKee numbering
 - more sophisticated numbering exists ...
 - re-numbering and re-meshing being expensive
 - ▶ the mesh should be kept constant on a time interval
 - ▶ AMR time-step computed through the **smallest block** and not the **smallest cell**
- $T_{n+1} - T_n = \Delta T_{\text{AMR}}$ is given by the CFL

$$\Delta T_{\text{AMR}} \leq \beta \frac{\min_k h_{\text{block}_k}}{\max_k \|\mathbf{u}_{\text{block}_k}\|}, \quad 0 < \beta \leq 1.$$



How it works ?

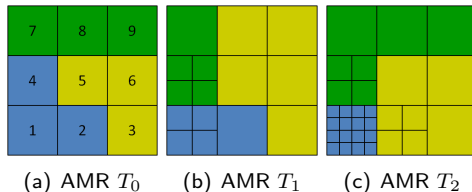
- each domain has almost the same number of cells
- domain are defined using Cuthill-McKee numbering
- more sophisticated numbering exists . . .
- re-numbering and re-meshing being expensive
 - ▶ the mesh should be kept constant on a time interval
 - ▶ AMR time-step computed through the **smallest block** and not the **smallest cell**
 - ▶ Gain is important and numerical stability is conserved !



Thomas Altazin, Mehmet Ersoy, Frédéric Golay, Damien Sous, and Lyudmyla Yushchenko. *Numerical entropy production for multidimensional conservation laws using Block-Based Adaptive Mesh Refinement scheme*. preprint, 2015.

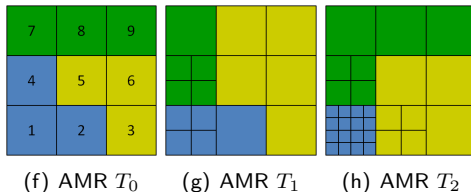
EXAMPLES :

- A two dimensional example of BB-AMR with 3 domains and 9 blocks.

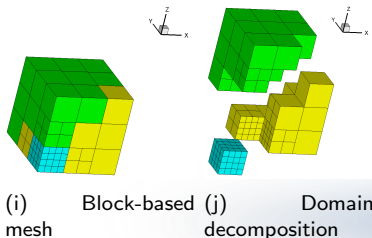


EXAMPLES :

- A two dimensional example of BB-AMR with 3 domains and 9 blocks.



- A three dimensional example of BB-AMR with 3 domains and 27 blocks.



1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

- Understanding of wave hydrodynamics is of primary interest for ocean and naval engineering applications :
 - ▶ dynamics of ships and floating structures,
 - ▶ stability of offshore structures,
 - ▶ coastal erosion and submersion processes,

- Understanding of wave hydrodynamics is of primary interest for ocean and naval engineering applications :
- It's difficult to describe accurately wave dynamics and still a fairly open research field.

breaking or impacting waves on rigid structures = violent transformations

- Understanding of wave hydrodynamics is of primary interest for ocean and naval engineering applications :
- It's difficult to describe accurately wave dynamics and still a fairly open research field.
- involved physical processes, such as splash-ups or gas pockets entrapment, are quite complex and can hardly be characterized by field or laboratory experiments or analytical approaches : **several models !** :

- Understanding of wave hydrodynamics is of primary interest for ocean and naval engineering applications :
- It's difficult to describe accurately wave dynamics and still a fairly open research field.
- involved physical processes, such as splash-ups or gas pockets entrapment, are quite complex and can hardly be characterized by field or laboratory experiments or analytical approaches : several models ! :
- **Therefore**, numerical simulation of breaking and impacting waves is both
 - ▶ an attractive research topic
 - ▶ a challenging task for coastal and environmental engineering



1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

- Assumptions : physics of impacting/breaking waves can be simplified
 - ▶ mainly governed by pressure forces and overturning forces
 - ▶ Mach number < 0.3 \rightarrow fluid is slightly compressible

- Assumptions : physics of impacting/breaking waves can be simplified
 - ▶ mainly governed by pressure forces and overturning forces
 - ▶ Mach number $< 0.3 \rightarrow$ fluid is slightly compressible
 - ▶ small-scale friction and dissipation process are neglected

- Assumptions : physics of impacting/breaking waves can be simplified
 - mainly governed by pressure forces and overturning forces
 - Mach number $< 0.3 \rightarrow$ fluid is slightly compressible
 - small-scale friction and dissipation process are neglected
 - two-phase flow Compressible Euler equations can be considered
- Model (2D and 3D) : low mach two phase

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 \end{aligned} \quad \text{where} \quad \begin{array}{ll} \rho(t, x) & : \text{ density} \\ u(t, x) & : \text{ velocity} \\ p(t, x) & : \text{ pressure} \\ \varphi & : \text{ fluid's fraction} \end{array}$$

- Assumptions : physics of impacting/breaking waves can be simplified
 - mainly governed by pressure forces and overturning forces
 - Mach number $< 0.3 \rightarrow$ fluid is slightly compressible
 - small-scale friction and dissipation process are neglected
 - two-phase flow Compressible Euler equations can be considered
 - An artificial linearized pressure law is used to compute low Mach flows [C67]**
- Model (2D and 3D) : low mach two phase

$$\begin{aligned}
 \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\
 \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\
 \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0
 \end{aligned}
 \quad \text{where} \quad
 \begin{aligned}
 \rho(t, x) &: \text{density} \\
 u(t, x) &: \text{velocity} \\
 p(t, x) &: \text{pressure} \\
 \varphi &: \text{fluid's fraction}
 \end{aligned}$$

with $p = p_0 + c_0 (\rho - (\varphi \rho_w + (1 - \varphi) \rho_a))$



Chorin, A.J. . *A Numerical Method for Solving Incompressible Viscous Flow Problems*. Journal of Computational Physics 2 (1) : 12 – 26, 1967

THE GOVERNING EQUATIONS

- Assumptions
- Model (2D and 3D) : low mach two phase

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 \end{aligned} \quad \text{where} \quad \begin{array}{ll} \rho(t, x) & : \text{ density} \\ u(t, x) & : \text{ velocity} \\ p(t, x) & : \text{ pressure} \\ \varphi & : \text{ fluid's fraction} \end{array}$$

with $p = p_0 + c_0 (\rho - (\varphi \rho_w + (1 - \varphi) \rho_a))$

- Equation of state with artificial sound speed \rightarrow CFL less restrictive

THE GOVERNING EQUATIONS

- Assumptions
- Model (2D and 3D) : low mach two phase

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 \end{aligned} \quad \text{where} \quad \begin{array}{ll} \rho(t, x) & : \text{ density} \\ u(t, x) & : \text{ velocity} \\ p(t, x) & : \text{ pressure} \\ \varphi & : \text{ fluid's fraction} \end{array}$$

with $p = p_0 + c_0 (\rho - (\varphi \rho_w + (1 - \varphi) \rho_a))$

- Equation of state with artificial sound speed \rightarrow CFL less restrictive
- **Explicit scheme** \rightarrow easy parallel implementation (MPI)

- Assumptions
- Model (2D and 3D) : low mach two phase

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 \end{aligned} \quad \text{where} \quad \begin{array}{ll} \rho(t, x) & : \text{ density} \\ u(t, x) & : \text{ velocity} \\ p(t, x) & : \text{ pressure} \\ \varphi & : \text{ fluid's fraction} \end{array}$$

with $p = p_0 + c_0 (\rho - (\varphi \rho_w + (1 - \varphi) \rho_a))$

- Equation of state with artificial sound speed \rightarrow CFL less restrictive
- Explicit scheme \rightarrow easy parallel implementation (MPI)

✔ hyperbolic system

- Moreover,

- Assumptions
- Model (2D and 3D) : low mach two phase

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 \end{aligned} \quad \text{where} \quad \begin{array}{ll} \rho(t, x) & : \text{ density} \\ u(t, x) & : \text{ velocity} \\ p(t, x) & : \text{ pressure} \\ \varphi & : \text{ fluid's fraction} \end{array}$$

with $p = p_0 + c_0 (\rho - (\varphi \rho_w + (1 - \varphi) \rho_a))$

- Equation of state with artificial sound speed \rightarrow CFL less restrictive
- Explicit scheme \rightarrow easy parallel implementation (MPI)
 - ✓ hyperbolic system
 - ✓ entropy available
- Moreover,

- Assumptions
- Model (2D and 3D) : low mach two phase

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 \end{aligned} \quad \text{where} \quad \begin{array}{ll} \rho(t, x) & : \text{ density} \\ u(t, x) & : \text{ velocity} \\ p(t, x) & : \text{ pressure} \\ \varphi & : \text{ fluid's fraction} \end{array}$$

with $p = p_0 + c_0 (\rho - (\varphi \rho_w + (1 - \varphi) \rho_a))$

- Equation of state with artificial sound speed \rightarrow CFL less restrictive
- Explicit scheme \rightarrow easy parallel implementation (MPI)
 - ✓ hyperbolic system
 - ✓ entropy available
- Moreover,
 - ✓ automatic mesh refinement

- Assumptions
- Model (2D and 3D) : low mach two phase

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \operatorname{div}(\rho u) &= 0 \\ \frac{\partial \rho u}{\partial t} + \operatorname{div}(\rho u^2 + pI) &= \rho g \\ \frac{\partial \varphi}{\partial t} + u \cdot \nabla \varphi &= 0 \end{aligned} \quad \text{where} \quad \begin{array}{ll} \rho(t, x) & : \text{ density} \\ u(t, x) & : \text{ velocity} \\ p(t, x) & : \text{ pressure} \\ \varphi & : \text{ fluid's fraction} \end{array}$$

with $p = p_0 + c_0 (\rho - (\varphi \rho_w + (1 - \varphi) \rho_a))$

- Equation of state with artificial sound speed \rightarrow CFL less restrictive
- Explicit scheme \rightarrow easy parallel implementation (MPI)
 - ✓ hyperbolic system
 - ✓ entropy available
- Moreover,
 - ✓ automatic mesh refinement
 - ✓ local time stepping

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

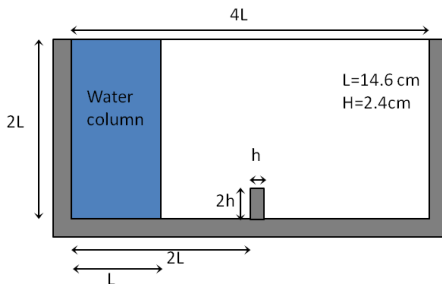
- capture the complex structure of the air-water interface after wave impact



Koshizuka, S., H. Tamako, and Y. Oka. *A particle method for incompressible viscous flow with fluid fragmentations*. Computational Fluid Dynamics Journal, 4 (1) : 29–46, 1995.

A TWO-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Experimental configuration



A TWO-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact

- Numerical parameters :

Mesh refinement parameter α_{\max}	: 0.2 ,
Mesh coarsening parameter α_{\min}	: 0.02 ,
Number of domain	: 321,
Number of blocks	: 321,
Number of processors	: 120,
Maximum level of mesh refinement	: $L_{\max} = 5$,
CFL	: $CFL = 0.8$,
Simulation time	: $T = 1.5$,
AMR time	: $AMR = 300$.

A TWO-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Confrontation with experiments : $T = 0$

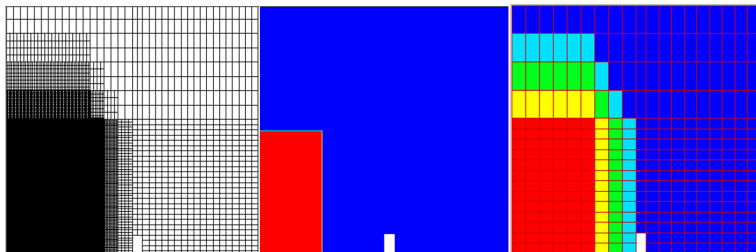


FIGURE: mesh (left), density with blue and red corresponding to air and water, respectively (center), mesh refinement level (1 to 5) per block (right)

A TWO-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Confrontation with experiments : $T = 0.2$

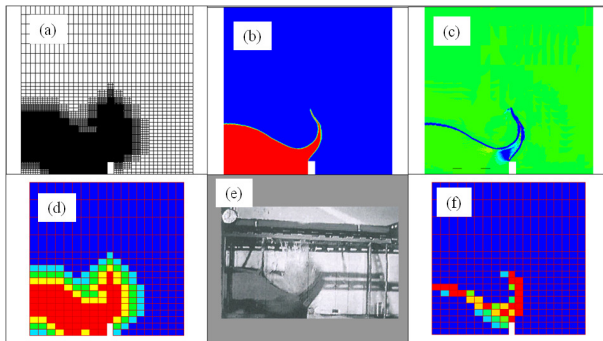


FIGURE: (a) Mesh ; (b) Density (air-blue, water-red) ; (c) Density of numerical entropy production (green-zero, blue-negative values) ; (d) Mesh refinement level per block (1 to 5) ; (e) Experiment ; (f) Mesh refinement criterion per block.

A TWO-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Confrontation with experiments : $T = 0.4$

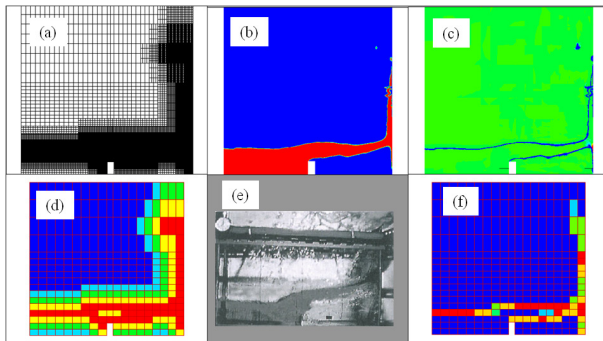


FIGURE: (a) Mesh ; (b) Density (air-blue, water-red) ; (c) Density of numerical entropy production (green-zero, blue-negative values) ; (d) Mesh refinement level per block (1 to 5) ; (e) Experiment ; (f) Mesh refinement criterion per block.

A TWO-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- **Remarks :**
 - ▶ number of cells varies from 70 000 and 100 000
 - ▶ elapsed computing time about 5 hours
 - ▶ 1 domain = 1 block \rightarrow better results with BB-AMR.

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

- capture the complex structure of the air-water interface after wave impact



Kleefsman, K.M.T., G. Fekken, A.E.P. Veldman, B. Iwanowski, and B. Buchner. *A Volume-of-Fluid based simulation method for wave impact problems*. Journal of Computational Physics 206 (1) : 363 – 393, 2005.

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Experimental configuration

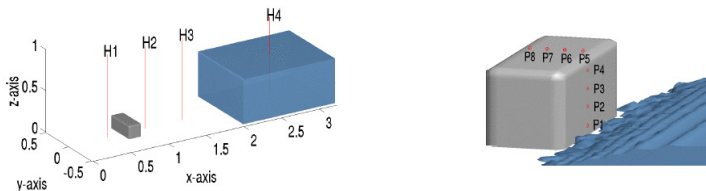


FIGURE: domain geometry and sensors points from
<http://www.math.rug.nl/~simonveldman/comflow/dambreak.html>

A THREE-DIMENSIONAL DAM-BREAK PROBLEM²

- capture the complex structure of the air-water interface after wave impact
- Numerical parameters :

Mesh refinement parameter α_{\max}	: 0.2 ,
Mesh coarsening parameter α_{\min}	: 0.02 ,
Number of domain	: 48,
Number of blocks	: 3628,
Number of processors	: 48,
Maximum level of mesh refinement	: $L_{\max} = 4$,
CFL	: $CFL = 0.8$,
Simulation time	: $T = 4.8$,
AMR time	: $AMR = 240$.

2. 48 Intel X5675 cores

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Confrontation with experiments :

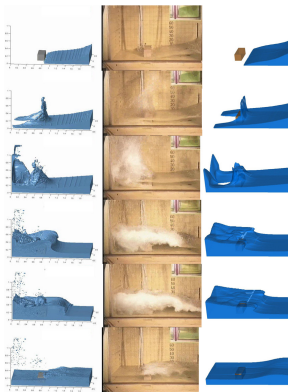
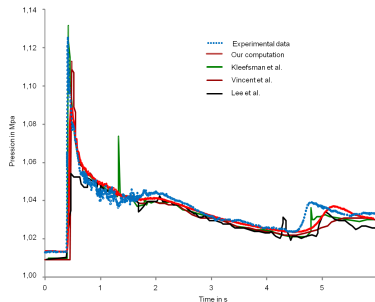
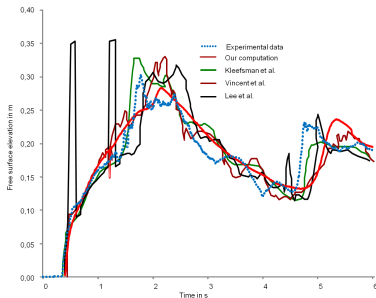


FIGURE: Free surface computed by Kleefsman (left), the experimentation (center) and our (right) at $t = 0.4, 0.6, 1, 1.8, 2, 4.8s$

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Confrontation with experiments :



Lee, E.S., D. Violeau, R. Issa, and S. Ploix. *Application of weakly compressible and truly incompressible SPH to 3-D water collapse in waterworks*. Journal of Hydraulic Research 48 (sup1) : 50–60, 2010.



Vincent, S., G. Balmigère, J.-P. Caltagirone, and E. Meillot. *Eulerian-Lagrangian multiscale methods for solving scalar equations - Application to incompressible two-phase flows*. Journal of Computational Physics 229 (1) : 73 – 106, 2010

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- Confrontation with experiments :

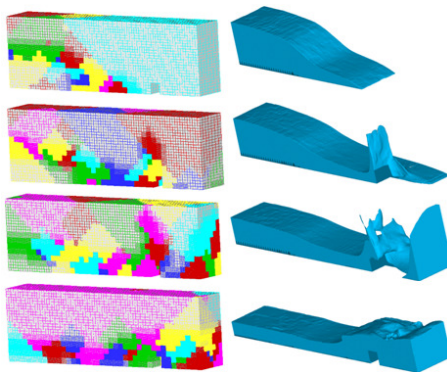


FIGURE: Domains due to the BB-AMR scheme (left) and air-water interface (right) at time $0.4s$, $0.6s$, $1.0s$, $2s$.

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- capture the complex structure of the air-water interface after wave impact
- **Remarks :**
 - ▶ number of cells varies from 800 000 cells up to about 1 500 000 cells
 - ▶ elapsed computing time about 10 hours (instead of 24h [GH07])



Golay, F., and P. Helluy. *Numerical schemes for low Mach wave breaking*. International Journal of Computational Fluid Dynamics 21(2) : 69–86, 2007.



YUSHCHENKO, L., GOLAY, F., ERSOY, M. *Production d'entropie et raffinement de maillage. Application au déferlement de vague*. 21ème Congrès Français de Mécanique, 26 au 30 août 2013, Bordeaux, France (FR).



Golay, F., Ersoy, M., Yushchenko, L., Sous, D. *Block-based adaptive mesh refinement scheme using numerical density of entropy production for three-dimensional two-fluid flows*. International Journal of Computational Fluid Dynamics 29.1, 67-81, 2015.

- A “block” dam break problem with a confrontation of RK2 and AB2



Thomas Altazin, Mehmet Ersoy, Frédéric Golay, Damien Sous, and Lyudmyla Yushchenko. *Numerical entropy production for multidimensional conservation laws using Block-Based Adaptive Mesh Refinement scheme*. preprint, 2015.

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- A “block” dam break problem with a confrontation of RK2 and AB2
- Initial configuration

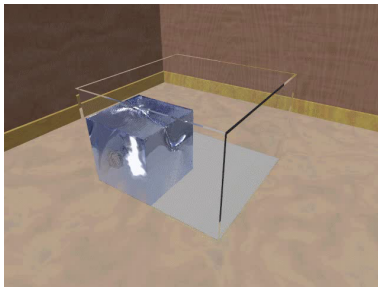


FIGURE: Unit cube $\left(\frac{1}{2} \times \frac{1}{2} \times \frac{1}{2}\right)$

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- A “block” dam break problem with a confrontation of RK2 and AB2
- Numerical parameters :

Mesh refinement parameter α_{\max}	: 0.2 ,
Mesh coarsening parameter α_{\min}	: 0.02 ,
Number of domain	: 1, 2, 4, 8, 32,
Number of blocks	: 3375,
Number of processors	: 40,
Maximum level of mesh refinement	: $L_{\max} = 4$,
Simulation time	: $T = 2.5$,
AMR time	: $AMR = 100$.

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- A “block” dam break problem with a confrontation of RK2 and AB2
- Confrontation with experiments :

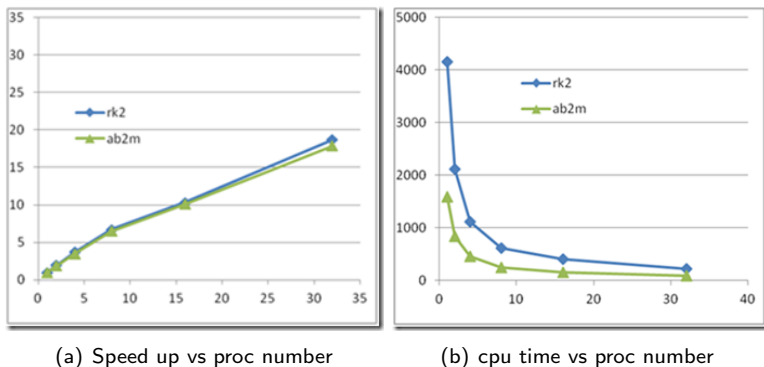


FIGURE: AB2 vs RK2

A THREE-DIMENSIONAL DAM-BREAK PROBLEM

- A “block” dam break problem with a confrontation of RK2 and AB2
- **Remarks :**
 - ▶ number of cells varies from 172215 cells up to about 587763 cells
 - ▶ The efficiency, i.e. $\frac{\text{speed up}}{\text{number of processors}}$, of the computation is roughly 85% for 8 domains and 60% for 32 domains.
 - ▶ performance decrease after 20 processors → optimization is required to get more efficiency.

1 PRINCIPLE OF THE METHOD

- Generality
- 1d examples and local time stepping
- Data structure : BB-AMR

2 APPLICATIONS

- The two phase low Mach model
- A two-dimensional dam-break problem
- A three-dimensional dam-break problem

3 CONCLUSIONS

CONCLUSIONS

- Several numerical validation on Euler equations

CONCLUSIONS

- Several numerical validation on Euler equations
- Several numerical validation (in progress) for shallow water equations

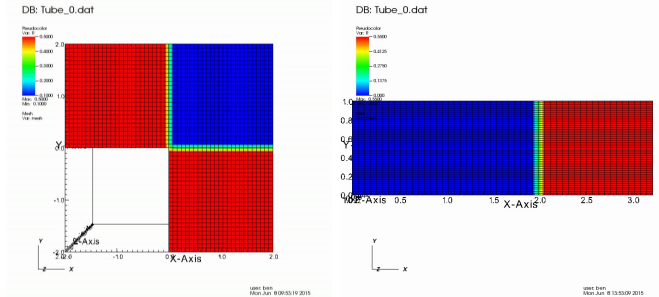


FIGURE: (left) L and (right) Kleefsman test case (B. Cleirec)

- Several numerical validation on Euler equations
- Several numerical validation (in progress) for shallow water equations
- local consistency error between two adjacent cells of different levels

- Several numerical validation on Euler equations
- Several numerical validation (in progress) for shallow water equations
- local consistency error between two adjacent cells of different levels
- capture accurately rarefactions and contact discontinuities

- Several numerical validation on Euler equations
- Several numerical validation (in progress) for shallow water equations
- local consistency error between two adjacent cells of different levels
- capture accurately rarefactions and contact discontinuities
- Develop a 'returning' wave model (as an intermediate one between the two-phase flow model and the shallow water equations)

A dynamic background image showing a large splash of water with many droplets in the air, creating a sense of movement and freshness. The water is a clear, light blue color.

Thank you

Thank you

for your

for your

attention

attention